

TITLE
ION DETECTOR

CROSS REFERENCE TO RELATED APPLICATION

5 This application claims priority from United States
Provisional Application 60/433,023, filed December 13,
2002 and United Kingdom Patent Application 0229001.3,
filed December 12, 2002. The contents of these
applications are incorporated herein by reference.

10

STATEMENT OF FEDERAL SPONSORED RESEARCH

N/A

FIELD OF INVENTION

15 The present invention relates to an ion detector
for use in a mass spectrometer, a mass spectrometer, a
method of detecting ions and a method of mass
spectrometry.

20

BACKGROUND OF INVENTION

Commercial high performance Time of Flight mass
spectrometers generally utilise ion detection systems
comprising microchannel plates for pre-amplifying ion
pulse signals. Microchannel plates generate multiple
25 electrons in response to an ion striking the input
surface of the microchannel plate. The electrons which
are generated by the microchannel plate provide an
amplified signal which may then be subsequently recorded
using a fast Analogue to Digital Converter ("ADC") or a
30 Time to Digital Converter ("TDC"). Ion detectors
comprising two microchannel plates are advantageously
used for amplification of ion pulse signals in Time of
Flight mass spectrometers.

Microchannel plate ion detectors are particularly advantageous for use in Time of Flight mass spectrometers since they provide a high gain amplification. For example, a single ion striking the input surface of a microchannel plate ion detector will typically cause several million electrons to be emitted from the output surface of the microchannel plate which can then be recorded. Microchannel plate ion detectors also have a relatively fast response time. Typically, an ion striking the input surface of a microchannel plate ion detector will generate a pulse of electrons having a pulse width of the order of a few nanoseconds at half pulse height. A further advantage of microchannel plate ion detectors is that the input surface of the microchannel plate is relatively flat and hence ions travel a relatively constant distance to the microchannel plate. Therefore, any spread in the arrival times of the ions at the input surface of the microchannel plate(s) is effectively negligible.

Although conventional microchannel plate ion detectors have several advantages they also have several disadvantages. In particular, conventional microchannel plate ion detectors suffer from signal induced ringing noise and/or reduced bandwidth caused by impedance mismatching between the collection anode which collects electrons from the microchannel plate(s) and the 50 Ω input amplifier of the Analogue to Digital Converter or the Time to Digital Converter used as part of the acquisition electronics. Another disadvantage of conventional microchannel plate ion detectors results from the requirement that Time of Flight mass

spectrometers are designed to mass analyse ions having relatively high kinetic energies, typically several keV. In order to achieve such relatively high ion kinetic energies the ions are normally accelerated through an electric field generated by a high voltage difference between the ion source and the field free drift tube of the Time of Flight mass analyser. The mass spectrometer may be configured, for example, such that the ion source is floated at a high voltage and the flight tube is grounded or vice versa. However, normally the input amplifier of an Analogue to Digital Converter or a Time to Digital Converter in the ion detector is required to be operated at ground potential. Therefore, in order to apply an appropriate bias voltage to accelerate the electrons from the microchannel plate(s) to the collection anode of the ion detector it may be necessary to capacitively decouple the collection anode from the input of the Analogue to Digital Converter or the Time to Digital Converter. However, conventional approaches to capacitively decoupling the collection anode from the Analogue to Digital Converter or the Time to Digital Converter cause impedance mismatching between the collection anode and the Analogue to Digital Converter or the Time to Digital Converter. A further disadvantage of conventional microchannel plate ion detectors is that the collection anode tends to capacitively pick up high frequency noise from nearby circuitry such as high voltage power supplies which are used to power the microchannel plate(s) or the collection anode.

The combined effects of signal induced ringing noise, reduced bandwidth and high frequency noise pick-up in conventional microchannel plate ion detectors are

detrimental to the mass resolving power and detection limits of the overall Time of Flight mass spectrometer. A further disadvantage of conventional microchannel plate ion detectors is that signal saturation may result from electron depletion in the microchannel plate(s) immediately after a relatively large ion pulse has been detected. This signal saturation results in a reduction of gain of the ion detector immediately after detection of a relatively large ion pulse.

It is therefore further desired to provide an improved microchannel plate ion detector.

SUMMARY OF THE INVENTION

According to an aspect of the present invention there is provided an ion detector for use in a mass spectrometer, the ion detector comprising: one or more microchannel plates, wherein in use ions are received at an input surface of the one or more microchannel plates and electrons are released from an output surface of the one or more microchannel plates; and an anode having a surface upon which electrons are received in use; wherein the ion detector further comprises: one or more electrodes and/or one or more magnetic lenses which, in use, direct, guide or attract at least some of the electrons released from the output surface of the one or more microchannel plates onto the anode; and wherein the output surface of the one or more microchannel plates has a first area and the surface of the anode has a second area, wherein the second area is $\geq 5\%$ of the first area.

The one or more electrodes and/or the one or more magnetic lenses may be arranged between the one or more microchannel plates and the anode. The one or more

electrodes and/or the one or more magnetic lenses may alternatively/additionally be arranged so as to surround at least a portion of the anode.

5 The one or more magnetic lenses preferably comprise one or more electro-magnets and/or one or more permanent magnets.

The anode may be made from a non-magnetic material. However, more preferably, the anode may be made from a soft (low coercivity) magnetic material. A soft
10 magnetic material may be considered to have a coercivity (H_c) less than about 1000 Amp/meter. According to another embodiment the anode may be made from a hard or permanent (high coercivity) magnetic material. A hard magnetic material may be considered to have a coercivity
15 of at least 3000, 3500 or 4000 Amp/meter.

The second area of the anode is preferably 5-90% of the first area of the output surface of the one or more microchannel plates. For example, the second area may be $\leq 85\%$, $\leq 75\%$, $\leq 70\%$, $\leq 65\%$, $\leq 60\%$, $\leq 55\%$, $\leq 50\%$, $\leq 45\%$, $\leq 40\%$, $\leq 35\%$, $\leq 30\%$, $\leq 25\%$, $\leq 20\%$, $\leq 15\%$ or $\leq 10\%$
20 of the first area.

The second area may be $\geq 10\%$, $\geq 15\%$, $\geq 20\%$, $\geq 25\%$, $\geq 30\%$, $\geq 35\%$, $\geq 40\%$, $\geq 45\%$, $\geq 50\%$, $\geq 55\%$, $\geq 60\%$, $\geq 65\%$, $\geq 70\%$, $\geq 75\%$, $\geq 80\%$ or $\geq 85\%$ of the first area.

25 Preferably, the one or more electrodes comprise one or more ring lenses. The one or more electrodes may be relatively thin for example having a thickness of ≤ 1.5 mm, ≤ 1.0 mm or ≤ 0.5 mm.

Alternatively/additionally, the one or more
30 electrodes may comprise one or more Einzel lens arrangements comprising three or more electrodes, one or more segmented rod sets, one or more tubular electrodes or one or more quadrupole rod sets. The one or more

electrodes may comprise a plurality of electrodes having apertures through which electrons are transmitted in use, the apertures having substantially the same area. Alternatively, the one or more electrodes may comprise a plurality of electrodes having apertures through which electrons are transmitted in use, the apertures becoming progressively smaller or larger in a direction towards the anode.

According to another aspect of the present invention there is provided an ion detector for use in a mass spectrometer, the ion detector comprising: one or more microchannel plates, wherein in use ions are received at an input surface of the one or more microchannel plates and electrons are released from an output surface of the one or more microchannel plates; and an anode having a surface upon which electrons are received in use; wherein the ion detector further comprises: one or more electro-magnets and/or one or more permanent magnets which, in use, direct or guide at least some of the electrons released from the output surface of the one or more microchannel plates onto the anode.

According to another aspect there is provided an ion detector for use in a mass spectrometer, the ion detector comprising: one or more microchannel plates, wherein in use ions are received at an input surface of the one or more microchannel plates and electrons are released from an output surface of the one or more microchannel plates; and an anode having a surface upon which electrons are received in use; wherein the ion detector further comprises: a plurality of electrodes and/or one or more magnetic lenses which, in use, direct, guide or attract at least some of the electrons

released from the output surface of the one or more microchannel plates onto the anode, wherein the output surface of the one or more microchannel plates has a first area and the surface of the anode has a second area.

The anode may in one embodiment comprise a pin anode.

The output surface of the one or more microchannel plates is preferably maintained at a first potential, the surface of the anode is preferably maintained at a second potential and the one or more of the electrodes and/or the one or more magnetic lenses are preferably maintained at a third potential.

The second potential may be more positive than the first potential. For example, the potential difference between the surface of the anode and the output surface of the one or more microchannel plates may be 0-50 V, 50-100 V, 100-150 V, 150-200 V, 200-250 V, 250-300 V, 300-350 V, 350-400 V, 400-450 V, 450-500 V, 500-550 V, 550-600 V, 600-650 V, 650-700 V, 700-750 V, 750-800 V, 800-850 V, 850-900 V, 900-950 V, 950-1000 V, 1.0-1.5 kV, 1.5-2.0 kV, 2.0-2.5 kV, > 2.5 kV or < 10 kV.

The third potential may be substantially equal to the first and/or the second potential. Alternatively, the third potential may be more positive than the first and/or the second potential. For example, the potential difference between the third potential and the first and/or the second potential may be 0-50 V, 50-100 V, 100-150 V, 150-200 V, 200-250 V, 250-300 V, 300-350 V, 350-400 V, 400-450 V, 450-500 V, 500-550 V, 550-600 V, 600-650 V, 650-700 V, 700-750 V, 750-800 V, 800-850 V, 850-900 V, 900-950 V, 950-1000 V, 1.0-1.5 kV, 1.5-2.0 kV, 2.0-2.5 kV, > 2.5 kV or < 10 kV. According to

another embodiment the third potential may be more negative than the first and/or the second potential. The third potential may in one embodiment be intermediate the first and second potentials.

5 The surface of the anode may be arranged a distance < 5 mm, 5-10 mm, 10-15 mm, 15-20 mm, 20-25 mm, 25-30 mm, 30-35 mm, 35-40 mm, 40-45 mm, 45-50 mm, 50-55 mm, 55-60 mm, 60-65 mm, 65-70 mm, 70-75 mm or > 75 mm from the output surface of the one or more microchannel plates.

10 According to another aspect of the present invention there is provided an ion detector for use in a mass spectrometer, the ion detector comprising: one or more microchannel plates, wherein in use ions are received at an input surface of the one or more
15 microchannel plates and electrons are released from an output surface of the one or more microchannel plates; and an anode having a surface upon which electrons are received in use; wherein the surface of the anode is arranged a distance x mm from the output surface and
20 wherein x is selected from the group consisting of: (i) 35-40 mm; (ii) 40-45 mm; (iii) 45-50 mm; (iv) 50-55 mm; (v) 55-60 mm; (vi) 60-65 mm; (vii) 65-70 mm; (viii) 70-75 mm; and (ix) > 75 mm; and wherein the output surface has a first area and the surface of the anode has a
25 second area.

 According to another aspect of the present invention there is provided an ion detector for use in a mass spectrometer, the ion detector comprising: one or more microchannel plates, wherein in use ions are
30 received at an input surface of the one or more microchannel plates and electrons are released from an output surface of the one or more microchannel plates, the output surface having a first area; and an anode

having a surface upon which electrons are received in use, wherein the surface of the anode has a second area; wherein the second area is 5-25% of the first area.

According to another aspect of the present
5 invention there is provided an ion detector for use in a mass spectrometer, the ion detector comprising: one or more microchannel plates, wherein in use ions are received at an input surface of the one or more
10 microchannel plates and electrons are released from an output surface of the one or more microchannel plates, the output surface having a first area; and an anode having a surface upon which electrons are received in use, wherein the surface of the anode has a second area; wherein the second area is 30-90% of the first area.

15 According to the preferred embodiment electrons may be received across substantially the whole of the second area.

The anode preferably comprises a first portion, a second portion and an electrically insulating layer
20 provided between the first and second portions, the first portion having a surface upon which electrons are received in use. The first portion may be maintained at a different DC potential to the second portion. Alternatively, the first portion may be maintained at
25 substantially the same DC potential as the second portion.

The anode is preferably substantially conical. A substantially conical screen may surround at least a portion of the anode. The anode preferably has a
30 capacitance of 0.01-0.1 pF, 0.1-1 pF, 1-10 pF or 10-100 pF. The surface of the anode upon which electrons are received in use is preferably substantially flat.

According to another aspect of the present invention there is provided a mass spectrometer comprising an ion detector as described above.

5 The mass spectrometer preferably comprises a Time of Flight mass analyser such as an axial or orthogonal acceleration Time of Flight mass analyser. The Time of Flight mass analyser may comprise a reflectron. The mass spectrometer may comprise an Analogue to Digital Converter ("ADC") or Time to Digital Converter ("TDC")
10 connected to the ion detector.

The mass spectrometer may comprise an Atmospheric Pressure Chemical Ionisation ("APCI") ion source, an Atmospheric Pressure Photo Ionisation ("APPI") ion source, a Laser Desorption Ionisation ("LDI") ion
15 source, an Inductively Coupled Plasma ("ICP") ion source, a Fast Atom Bombardment ("FAB") ion source, a Liquid Secondary Ions Mass Spectrometry ("LSIMS") ion source, a Field Ionisation ("FI") ion source, a Field Desorption ("FD") ion source, an Electron Impact ("EI")
20 ion source or a Chemical Ionisation ("CI") ion source.

More preferably, the mass spectrometer may comprises a Matrix Assisted Laser Desorption Ionisation ("MALDI") or Electrospray ion source.

The ion source may be continuous or pulsed.

25 According to another aspect of the present invention there is provided a method of detecting ions comprising: receiving ions at an input surface of one or more microchannel plates; releasing electrons from an output surface of the one or more microchannel plates;
30 and directing or guiding at least some of the electrons released from the one or more microchannel plates onto a surface of an anode by means of one or more electrodes and/or one or more magnetic lenses, wherein the area of

the surface of the anode is $\geq 5\%$ of the area of the output surface of the one or more microchannel plates.

According to another aspect of the present invention there is provided a method of detecting ions comprising: receiving ions at an input surface of one or more microchannel plates; releasing electrons from an output surface of the one or more microchannel plates; and directing or guiding at least some of the electrons released from the one or more microchannel plates onto a surface of an anode by means of one or more electro- magnets and/or one or more permanent magnets.

According to another aspect of the present invention there is provided a method of detecting ions comprising: receiving ions at an input surface of one or more microchannel plates; releasing electrons from an output surface of the one or more microchannel plates; directing or guiding at least some of the electrons released from the one or more microchannel plates onto a surface of an anode by means of a plurality of electrodes and/or one or more magnetic lenses.

According to another aspect of the present invention there is provided a method of detecting ions comprising: receiving ions at an input surface of one or more microchannel plates; releasing electrons from an output surface of the one or more microchannel plates; and directing at least some of the electrons released from the one or more microchannel plates onto a surface of an anode, wherein the surface of the anode is arranged a distance x mm from the output surface and wherein x is selected from the group consisting of: (i) 35-40 mm; (ii) 40-45 mm; (iii) 45-50 mm; (iv) 50-55 mm; (v) 55-60 mm; (vi) 60-65 mm; (vii) 65-70 mm; (viii) 70-75 mm; and (ix) > 75 mm.

According to another aspect of the present invention there is provided a method of detecting ions comprising: receiving ions at an input surface of one or more microchannel plates; releasing electrons from an output surface of the one or more microchannel plates; and directing at least some of the electrons released from the one or more microchannel plates onto a surface of an anode, wherein the area of the surface of the anode is 5-25% of the area of the output surface of the one or more microchannel plates.

According to another aspect of the present invention there is provided a method of detecting ions comprising: receiving ions at an input surface of one or more microchannel plates; releasing electrons from an output surface of the one or more microchannel plates; and directing at least some of the electrons released from the one or more microchannel plates onto a surface of an anode, wherein the area of the surface of the anode is 30-90% of the area of the output surface of the one or more microchannel plates.

According to another aspect of the present invention there is provided a method of mass spectrometry comprising a method of detecting ions as described above.

According to another aspect of the present invention there is provided an ion detector for use in a mass spectrometer, the ion detector comprising: one or more microchannel plates, wherein in use ions are received at an input surface of the one or more microchannel plates and electrons are released from an output surface of the one or more microchannel plates, the output surface having a first area; and an anode having a surface upon which electrons are received in

use, the surface having a second area; wherein the anode comprises a hard or permanent magnetic material so that at least some of the electrons released from the output surface of the one or more microchannel plates are
5 directed or guided onto the anode.

The hard or permanent magnetic material preferably has a coercivity (H_c) of at least 3000, 3500 or 4000 Amp/meter.

The anode preferably generates a magnetic field and
10 wherein at least some of the electrons released from the output surface of the one or more microchannel plates are subject to the Lorentz force due to the magnetic flux from the anode and follow a substantially curved trajectory towards the anode with axial and angular
15 components relative to the direction of the magnetic flux. Alternatively, it may be considered that the anode generates a magnetic field wherein at least some of the electrons released from the output surface of the one or more microchannel plates spiral around lines of
20 magnetic field towards the anode.

At least 50%, 60%, 70%, 80%, 90% or 95% of the electrons released from the output surface of the one or more microchannel plates preferably have an energy of ≤ 500 eV, ≤ 450 eV, ≤ 400 eV, ≤ 350 eV, ≤ 300 eV, ≤ 250
25 eV, ≤ 200 eV, ≤ 150 eV, ≤ 100 eV or ≤ 50 eV. At least 50%, 60%, 70%, 80%, 90% or 95% of the electrons released from the output surface of the one or more microchannel plates preferably have an energy of ≥ 1 eV, ≥ 2 eV, ≥ 5 eV, ≥ 10 eV, ≥ 20 eV or ≥ 50 eV.

30 The potential difference between the surface of the anode and the output surface of the one or more microchannel plates is preferably 0-1 V, 1-5 V, 5-10 V,

10-15 V, 15-20 V, 20-25 V, 25-30 V, 30-50 V, 50-100 V, >
100 V or < 100 V.

According to another aspect of the present invention there is provided a method of detecting ions
5 comprising: receiving ions at an input surface of the one or more microchannel plates; releasing electrons from an output surface of the one or more microchannel plates; and directing or guiding at least some of the electrons released from the one or more microchannel
10 plates onto a surface of an anode, the anode comprising a hard or permanent magnetic material.

According to another aspect of the present invention there is provided a method of mass spectrometry comprising a method of detecting ions as
15 described above.

The ion detector according to the preferred embodiment is capable of detecting either positive or negative ions. The preferred ion detector may be incorporated into a Time of Flight mass spectrometer
20 comprising an ion source and a field free flight tube operated at a high voltage. The preferred ion detector comprises a collection anode which has a reduced capacitance and which is preferably capacitively decoupled from the microchannel plate(s). The preferred
25 ion detector may also comprise a lens system arranged between the microchannel plate(s) and the collection anode for focusing and screening electrons which leave the output surface of the microchannel plate(s).

The preferred embodiment relates to a microchannel
30 plate ion detector assembly which is capable of detecting either positive or negative ions without imposing limitations on the voltages which are applied to various components of the Time of Flight mass

spectrometer upstream of the ion detector. The preferred ion detector also preferably has a relatively large bandwidth, reduced ringing noise and exhibits reduced capacitative pick-up of high frequency electronic noise.

The frequency of ringing noise observed using a microchannel plate ion detector may be approximated by:

$$f = \frac{1}{2\pi\sqrt{LC}}$$

10

where f is the ringing noise frequency in Hertz, L is the stray inductance in the collection anode circuitry in Henrys and C is the capacitance between the microchannel plate and the collection anode in Farads.

15

The ringing noise frequency f increases as the capacitance C between the microchannel plate and collection anode decreases. Provided that the ringing noise frequency is high enough, the analogue bandwidth (typically 500 MHz) of the amplifier in the Time to Digital Converter or the Analogue to Digital Converter will significantly attenuate the intensity of the ringing noise. Therefore, by decreasing the capacitance between the collection anode and the microchannel plate the ringing noise in the ion detector may be reduced.

20

25

In a conventional microchannel plate ion detector the microchannel plate(s) are circular and have the same diameter as a circular collection anode located behind the microchannel plate(s). The microchannel plate(s) are also positioned in relatively close proximity to the collection anode i.e. they are separated by about 5-10 mm. This conventional ion detector arrangement provides an assembly having a relatively high capacitance between the collection anode and microchannel plate(s).

30

It is known to make the collection anode conical in shape in an attempt to maintain the 50 Ω impedance matching between the collection anode and the coaxial amplifier cable leading to either the Time to Digital Converter or the Analogue to Digital Converter. In a conventional microchannel plate ion detector the capacitance C_1 between the collection anode and the microchannel plate(s) in Farads may be approximated as follows:

$$C_1 = \frac{\epsilon\pi\left(\frac{D_1}{2}\right)^2}{G_1}$$

where ϵ is the permittivity of a vacuum (8.854×10^{-12} F/m), D_1 is the diameter of the surface of the circular collection anode and G_1 is the distance between the collection anode and the output surface of the rearmost circular microchannel plate(s).

In the preferred embodiment of the present invention the capacitance between the microchannel plate and collection anode is significantly reduced by increasing the distance between the microchannel plate(s) and the collection anode and/or decreasing the size of the surface of the collection anode. The capacitance C_2 between a circular collection anode and a circular microchannel plate(s) may be approximated as:

$$C_2 = \frac{\epsilon\pi\left(\frac{D_2}{2}\right)^2}{G_2}$$

where D_2 is the diameter of the circular surface of the collection anode and G_2 is the distance between the

collection anode and the output face of the microchannel plate(s).

The ratio of capacitance C_2 between the collection anode and microchannel plate(s) according to the preferred embodiment to the capacitance C_1 between the collection anode and microchannel plate(s) of a conventional ion detector is given by:

$$\frac{C_2}{C_1} = \frac{G_1}{G_2} \left(\frac{D_2}{D_1} \right)^2$$

For example, if a conventional ion detector has a distance G_1 of 5 mm between the collection anode and the microchannel plate(s) and the collection anode has a circular surface with a diameter D_1 of 50 mm then the capacitance between the collection anode and the microchannel plate(s) is 3.5 pF. However, if the diameter D_2 of the surface of the collection anode is reduced to 25 mm and the distance G_2 between the collection anode and microchannel plate(s) is also increased to 25 mm then the capacitance C_2 between the collection anode and microchannel plate(s) is significantly reduced to 0.17 pF. In this example the effect of reducing the size of the surface of the collection anode and of increasing the spacing between the collection anode and the microchannel plate(s) is to reduce the capacitance between the collection anode and the microchannel plate(s) by a factor of x20. Accordingly, the ringing noise frequency f will increase by a factor of approximately x4 and hence provided the ringing noise frequency is high enough the amplifier of the Analogue to Digital Converter or the Time to Digital

Converter will significantly attenuate the ringing noise.

The reduction in capacitance between the preferred collection anode and the microchannel plate(s) also
5 advantageously provides a significant reduction in the level of electronic noise pick-up and impedance mismatch between the collection anode and the co-axial cable leading to the Analogue to Digital Converter or to the Time to Digital Converter.

10 In the preferred embodiment the ion detector comprises one or more microchannel plates with the collection anode arranged downstream of the microchannel plate(s). The microchannel plate(s) receive ions at an input surface and generate electrons which are released
15 from an output surface. The electrons emitted from the microchannel plates are collected by a collection anode.

A lens system may be arranged between the microchannel plate(s) and the collection anode. In one embodiment the lens system may direct or guide electrons
20 from the output surface of the microchannel plate(s) to the input surface of the collection anode. This enables the voltage difference between the microchannel plate(s) and the collection anode to be reduced whilst still transferring the electrons from the microchannel
25 plate(s) to the collection anode efficiently. The lens system also enables electrons to be directed or guided to the collection anode with negligible spreading in the electron flight times by the anode. The lens system also preferably reduces the detrimental effect of
30 electric fields penetrating into the region between the microchannel plate(s) and collection electrode. This is a particular problem when a microchannel plate ion detector is used in a Time of Flight mass spectrometer

wherein the flight tube of the Time of Flight mass spectrometer is floated at a relatively high voltage.

In another embodiment the lens system may be operated in a defocusing mode in order to control the overall gain of the ion detector or to blank out amplified signals which are likely to saturate a detection system which includes a Time to Digital Converter. The lens system may also be operated in a defocusing mode so that electrons that are released from certain areas of the microchannel plate are selectively directed or guided to the collection anode. For example, the lens system may guide electrons released from the centre of the microchannel plate to the collection anode whilst blocking electrons released from the periphery of the microchannel plate. This may be advantageous in that ions striking the centre of the input surface of the microchannel plate may generate pulses of electrons which are separated in time with a greater resolution compared with pulses of electrons generated in response to ions striking the periphery of the microchannel plate.

In one embodiment the lens system may comprise a plurality of ring lens elements. The ring lens elements are preferably conductive metal rings and preferably have relatively small surface areas so that any capacitive coupling between the microchannel plate(s) and the collection anode is minimised. The ring lens elements are preferably relatively thin (e.g. ≤ 0.5 mm) to help reduce capacitive coupling of high frequency noise onto the collection anode. The ring lens elements may also be connected to separate individual voltage supplies in order to reduce coupling between the individual ring lens elements and hence therefore

between the microchannel plate(s) and the collection anode. Alternatively, the ring lens elements may be connected to a common voltage supply with each ring lens element being insulated from the other ring lens elements by high value resistors so that coupling between the ring lens elements is reduced.

According to an embodiment the collection anode is itself constructed as a capacitor in order to decouple the collection anode, which may be maintained at a relatively high voltage, from the Analogue to Digital Converter or from the Time to Digital Converter that records the signal generated by an ion arrival at the input surface of a double microchannel plate arrangement.

Various embodiments of the present invention together with other arrangements given for illustrative purposes only will now be described, by way of example only, and with reference to the accompanying drawings in which:

Fig. 1 shows a conventional microchannel plate ion detector;

Fig. 2 shows a microchannel plate ion detector according to a preferred embodiment;

Fig. 3 shows a collection anode according to a preferred embodiment comprising two portions separated by an electrically insulating layer;

Fig. 4 shows a simulation of the electric potentials and electron trajectories for a conventional ion detector;

Fig. 5 shows a simulation of the electric potentials and electron trajectories according to a preferred embodiment wherein a potential difference of

-13kV is maintained between the rearmost microchannel plate and the collection anode;

Fig. 6A shows a simulation of the electric potentials and electron trajectories according to a less preferred embodiment wherein a potential difference of
5 -50 V is maintained between the rearmost microchannel plate and the collection anode and Fig. 6B shows a simulation of the electric potentials and electron trajectories according to a preferred embodiment wherein
10 an intermediate focusing lens system is provided;

Fig. 7A shows a simulation of the electric potentials and electron trajectories according to a less preferred embodiment wherein a potential difference of
15 58 kV is maintained between the rearmost microchannel plate and the front portion of the collection anode and Fig. 7B shows a simulation of the electric potentials and electron trajectories according to a preferred embodiment wherein an intermediate lens system is provided and a potential difference of 750 V is
20 maintained between the rearmost microchannel plate and the front portion of the collection anode;

Fig. 8A shows a mass spectrum obtained using a conventional ion detector and which suffers from ringing noise and Fig. 8B shows a comparable mass spectrum
25 obtained using an ion detector according to the preferred embodiment which shows a significant reduction in ringing noise and which reveals the presence of a further mass peak which is not discernable from the conventional mass spectrum;

30 Fig. 9 shows a mass spectrum obtained using a preferred ion detector;

Fig. 10 shows an embodiment of an ion detector comprising a magnetic lens comprising an electro-magnet; and

Fig. 11 shows an embodiment of an ion detector
5 comprising a permanently magnetised anode.

DETAILED DESCRIPTION

A conventional microchannel plate ion detector 1 is shown in Fig. 1 and comprises two microchannel plates
10 3a,3b arranged to receive ions 7 from a flight tube 2 of a Time of Flight mass analyser. The two microchannel plates 3a,3b are arranged in contact with each other and with the channels of the two microchannel plates being angled with respect to the interface between the
15 microchannel plates 3a,3b. Ions 7 arriving at the ion detector 1 strike an input surface of the first microchannel plate 3a causing multiple electrons to be generated by the microchannel plate 3a. These electrons cause further cascading of electrons from the second
20 microchannel plate 3b. The electrons generated by the microchannel plates 3a,3b then exit the rearmost microchannel plate 3b and are subsequently collected by a conical collection anode 4 arranged slightly downstream of (i.e. 5-10 mm from) the rearmost
25 microchannel plate 3b. The output surface of the rearmost of the two microchannel plates 3b and the input surface of the collection anode 4 are circular and have substantially the same diameter D_1 and therefore have substantially the same area. The output surface of the
30 rearmost of the microchannel plates 3b and the input surface of the collection anode 4 are positioned relatively close to one other at a distance G_1 . The collection anode 4 is connected to a 50 Ω coaxial cable

6 which is connected to an Analogue to Digital Converter. A grounded conical screen 5 is provided radially outward from the collection anode 4.

Fig. 2 shows an ion detector 1' according to a preferred embodiment of the present invention. The ion detector 1' comprises two microchannel plates 3a,3b arranged to receive ions 7 from, for example, the flight tube 2 of a Time of Flight mass analyser. The ion detector 1' comprises a collection anode 4 which is arranged downstream of the two microchannel plates 3a,3b. A lens system 8,9 is preferably provided between the two microchannel plates 3a,3b and the collection anode 4. The collection anode 4 may be connected, for example, to an Analogue to Digital Converter or to a Time to Digital Converter by a coaxial cable 6. The input surface of the collection anode 4 is preferably substantially smaller than the output surface of the rearmost of the microchannel plates 3b. The output surface of the rearmost microchannel plate 3b and the input surface of the collection anode 4 are both preferably circular having diameters of D_1 and D_2 respectively, wherein preferably $D_1 > D_2$.

The collection anode 4 is arranged at a distance G_2 which is preferably further away from the rearmost microchannel plate 3b than the corresponding anode 4 in a conventional ion detector 1 as can be seen by comparing Figs. 1 and 2. The reduced surface area of the collection anode 4 according to the preferred embodiment and the increased distance G_2 of the collection anode 4 according to the preferred embodiment from the two microchannel plates 3a,3b significantly reduces the capacitance between the collection anode 4 and the two microchannel plates 3a,3b. This has the

effect of increasing the frequency of ringing noise in the ion detector 1'. The size of the collection anode 4 and the distance G_2 of the anode 4 from the two microchannel plates 3a,3b is preferably selected so that the frequency of the ringing noise is high enough so that it is significantly attenuated by an amplifier either in an Analogue to Digital Converter or a Time to Digital Converter connected to the ion detector 1'.

As shown in Fig. 2, according to the preferred embodiment a lens system 8,9 is preferably arranged between the two microchannel plates 3a,3b and the collection anode 4. The lens system 8 may comprise a plurality of relatively thin conductive ring lens elements. The ring lens elements may be made from metal and are preferably maintained at appropriate voltages so that electrons are electrostatically guided from the output face of the two microchannel plates 3a,3b onto the input surface of the relatively small collection anode 4. The lens system 8,9 preferably reduces the potential difference which would otherwise be required to be maintained between the rearmost microchannel plate 3b and the collection anode 4 in order to transfer electrons efficiently from the microchannel plates 3a,3b to the collection anode 4. The particular voltages which are applied to the ring lens elements of the lens system 8,9 will preferably depend upon the voltages applied to other components of the Time of Flight mass analyser arranged upstream of the ion detector 1' and will also depend upon the polarity of the ions 7. The lens system 8,9 preferably also has the effect of reducing any electric field penetration into the region between the two microchannel plates 3a,3b and the collection anode 4 which would otherwise be detrimental

to the efficient transferral of electrons from the microchannel plates 3a,3b to the collection anode 4. This is particularly advantageous when the ion detector forms part of a Time of Flight mass analyser and the two microchannel plates 3a,3b are floated at relatively high voltages.

The lens system 8,9 may also increase the energy of the electrons released from the rearmost microchannel plate 3b so that the electrons emitted from the microchannel plates 3a,3b travel to the collection anode 4 in a relatively short time. In this manner the lens system 8,9 preferably ensures that there is negligible spreading of the flight times of the electrons from the microchannel plates 3a,3b to the collection anode 4.

Each ring lens element of the lens system 8,9 is preferably relatively thin (e.g. approximately ≤ 0.5 mm) in order to reduce coupling of high frequency noise onto the collection anode 4. The rearmost ring lens element 9 located closest to the collection anode 4 is preferably constructed from an annular sheet having a thickness ≤ 0.5 mm and is preferably comprised of an electrical conductor having a central hole to allow electrons to pass through to the collection anode 4.

According to a particularly preferred embodiment the collection anode 4 may be constructed as a capacitor in order to decouple the collection anode 4, which may be maintained at a relatively high voltage, from an Analogue to Digital Converter or a Time to Digital Converter connected to the ion detector 1' and which records the signal generated by ions arriving at the input surface of the two microchannel plates 3a,3b. Fig. 3 shows a collection anode 4 which may be used in a preferred ion detector. The collection anode 4 is

preferably constructed as a capacitor having a capacitance < 100 pF by forming the collection anode 4 from two portions 10,12 separated by an electrically insulating layer 11.

5 The first portion 10 of the collection anode 4 is preferably capacitively decoupled from the second portion 12 of the collection anode 4 by the electrical insulating layer 11. The first 10 and second 12 portions of the collection anode 4 may therefore be
10 maintained in use at different potentials. For example, the second portion 12 of the collection anode 4 which is connected to the recording device by a coaxial cable 6 is preferably grounded whilst the first portion 10 of the collection anode 4 may be maintained at a relatively
15 high potential. Maintaining the second portion 12 of the collection electrode 4 at ground potential enables the output electronics to be simplified and also eliminates noise which would otherwise occur when connecting a voltage source to the output portion of the
20 collection anode 4. The electrical insulator 11 which separates the first 10 and second 12 portions of the collection anode 4 may comprise a thin plastic sheet made, for example, from a material such as Kapton (RTM). The decoupling of the first portion 10 of the collection
25 anode 4 from the second portion 12 and hence the recording device is particularly preferred in Time of Flight mass spectrometers wherein various components may be maintained at various voltages. For example, if an ion source producing negative ions were grounded and a
30 field free flight tube were floated at a relatively high positive voltage then the electric field between the rearmost microchannel plate 3b and the input surface of the-grounded collection anode in a conventional ion

detector would either be of incorrect polarity or would be insufficient in terms of magnitude in order to transfer the electrons efficiently from the microchannel plates 3a,3b to the collection anode 4. In the
5 preferred embodiment the first portion 10 of the collection anode 4 is decoupled from the recording device so that the first portion 10 of the collection anode 4 may be maintained at a voltage which is such that electrons are transported efficiently from the
10 rearmost microchannel plate 3b to the first portion 10 of the collection anode 4.

An advantage of the preferred embodiment is that both ringing noise and the pick-up of electronic noise is significantly reduced. Accordingly, relatively low
15 abundance ion signals will no longer be masked by such noise. The gain of the two microchannel plates 3a,3b can therefore be set at a lower value than would otherwise be the case with conventional microchannel plate ion detectors. This is particularly advantageous
20 in applications where the dynamic range of quantitation is limited by microchannel plate saturation effects which occur, for example, with higher abundance ion signals in Gas Chromatography Time of Flight mass spectrometers. Since the gain of the two microchannel
25 plates preferably may be set relatively low, the number or rate at which ions arrive at the ion detector may advantageously be relatively high before saturation effects begin to occur.

Figs. 4 to 7B show simulations of electron
30 trajectories 13 between the microchannel plates 3a,3b and the collection anode 4 of both conventional ion detectors 1 and more and less preferred embodiments 1' of the present invention. The electron trajectories 13

were simulated using the SIMION charged particle ray tracing program. The electric potential contours are also shown on the simulations.

Fig. 4 shows a simulation of the electric potentials and electron trajectories 13 in a conventional ion detector 1. A double microchannel plate arrangement 3a,3b is shown having a first microchannel plate 3a for receiving ions from a field free flight tube 2 of a Time of Flight mass analyser and a second microchannel plate 3b which emits electrons towards a collection anode 4. Positive or negative ions were assumed to be produced by an ion source maintained at positive or minus 15 kV respectively. The ions were therefore accelerated towards the field free flight tube 2 which was maintained at 0 V. The microchannel plates 3a,3b are shown having circular input and output surfaces of a diameter of 50 mm. The input surface and the output surface of the microchannel plates 3a,3b were maintained at -2 kV and -50 V respectively in this simulation. A collection anode 4 was modelled as being arranged 10 mm downstream of the output surface of the microchannel plates 3a,3b and which received electrons over a circular area also of 50 mm in diameter. The collection anode 4 was grounded. A grounded conical screen 5 was modelled as being provided radially outward of the collection anode 4. The collection anode 4 and conical screen 5 were connected to a coaxial cable which was connected to a recording device. Although electrons can be seen to be transferred efficiently from the rearmost microchannel plate 3b to the collection anode 4, because the collection anode 4 is relatively large and is arranged relatively close to the microchannel plates 3a,3b then there will be a relatively high level

of capacitive coupling between the microchannel plates 3a,3b and the collection anode 4. This will result in a relatively high level of ringing noise in the ion detector 1.

5 Fig. 5 shows a simulation of the electric potentials and electron trajectories 13 in a less preferred ion detector 1' not having a lens system. Positive ions were modelled as being produced by an ion source maintained at 0 V. The positive ions were then
10 accelerated towards the field free flight tube 2 of a Time of Flight mass spectrometer which was maintained at -15 kV. The microchannel plates 3a,3b had circular input and output surfaces of a diameter of 50 mm. The input surface and output surface of the microchannel
15 plates 3a,3b were maintained at -15 kV and -13 kV respectively. A collection anode 4 was arranged 50 mm downstream (i.e. at a much greater separation than a conventional system) of the output surface of the rearmost microchannel plate 3b. The collection anode 4
20 comprised a first portion 10 separated from a second portion 12 by an insulating layer 11. The first portion 10 of the collection anode 4 received electrons over a circular reduced area of 25 mm in diameter. In this particular example the first portion 10 and the second
25 portion 12 of the collection anode 4 were both maintained at 0 V. A grounded conical screen 5 was modelled as being provided radially outward of the collection anode 4. In this embodiment the relatively high potential difference (-13 kV) maintained between
30 the rearmost microchannel plate 3b and the first portion 10 of the collection anode 4 enabled electrons to be transported efficiently from the rearmost microchannel plate 3b to the first portion 10 of the collection anode

4. Due to the relatively small and distant collection anode 4 the capacitance between the collection anode 4 and microchannel plates 3a,3b is significantly reduced. This will result in a corresponding reduction in the ringing noise detected by the ion detector 1' and will also reduce the impedance mismatching between the collection anode 4 and the recording device.

Fig. 6A shows a simulation of the electric potentials and electron trajectories 13 according to a less preferred embodiment. Positive or negative ions are modelled as being produced by an ion source maintained at positive or minus 15 kV respectively. The ions are accelerated towards the field free flight tube 2 of a Time of Flight mass spectrometer maintained at 0 V. The input and output surfaces of the microchannel plates 3a,3b are preferably circular and have a diameter of 50 mm. The input surface and output surface of the microchannel plates 3a,3b were modelled as being maintained at -2 kV and -50 V respectively. The collection anode 4 was modelled as being arranged 50 mm downstream of the output surface of the rearmost microchannel plate 3b. The collection anode 4 comprises a first portion 10 separated from a second portion 12 by an insulating layer 11. The first portion 10 of the collection anode 4 receives electrons over a reduced circular area of 25 mm in diameter. The first portion 10 and second portion 12 of the collection anode 4 were grounded. A grounded conical screen 5 was modelled as being provided radially outward of the collection anode 4. In this less preferred embodiment the collection anode 4 is relatively small and distant from the microchannel plates 3a,3b but only a relatively small potential difference (-50 V) is maintained between the

rearmost microchannel plate 3b and the first portion 10 of the collection anode 4. Accordingly, a relatively large fraction of the electrons emitted from the microchannel plates 3a,3b are not accelerated onto the first portion 10 of the collection anode 4 and hence electrons are not transmitted efficiently from the microchannel plates 3a,3b to the collection anode 4.

Fig. 6B shows a simulation of the electric potentials and electron trajectories 13 according to a preferred embodiment. The ion detector 1' is substantially the same as the ion detector 1' shown in Fig. 6A except that an additional lens system 8,9 is provided between the microchannel plates 3a,3b and the collection anode 4. The lens system 8,9 preferably comprises three or more relatively thin ring lens elements which may, in one embodiment, be maintained at -50 V (i.e. the same potential as the rearmost microchannel plate 3b) and wherein the final annular ring lens element 9 is maintained at 0 V. In this embodiment the lens system 8,9 focuses the electrons emitted from the rearmost microchannel plate 3b onto the first portion 10 of the collection anode 4. The lens system 8,9 enables the capacitance and potential difference between the microchannel plates 3a,3b and the collection anode 4 to be reduced whilst maintaining efficient transportation of electrons from the microchannel plates 3a,3b to the collection anode 4.

Fig. 7A shows a simulation of the electric potentials and electron trajectories 13 according to a less preferred embodiment. Negative ions were modelled as being produced by an ion source maintained at 0 V. The ions were accelerated towards the field free flight tube 2 of a Time of Flight mass analyser which was

maintained at 15 kV. The input and output surfaces of the microchannel plates 3a,3b were circular and had a diameter of 50 mm. The input surface and output surface of the microchannel plates 3a,3b were maintained at 15
5 kV and 17 kV respectively. The collection anode 4 was arranged 50 mm downstream of the output surface of the microchannel plates 3a,3b. The collection anode 4 preferably comprises a first portion 10 separated from a second portion 12 by an insulating layer 11. The first
10 portion 10 of the collection anode 4 was maintained at 75 kV and had a circular surface area of 25 mm in diameter. The second portion 12 of the collection anode 4 was grounded. A grounded conical screen 5 was modelled as being provided radially outward of the
15 collection anode 4. In this less preferred embodiment the electric field between the rearmost microchannel plate 3b (maintained at 17 kV), and the first portion 10 of the collection anode 4 (maintained at a higher positive potential of 75 kV) acts to accelerate
20 electrons towards the collection anode 4. However, the electric field between the rearmost microchannel plate 3b and the second portion 12 of the collection anode 4 which is maintained at ground potential also acts to accelerate electrons back towards the rearmost
25 microchannel plate 3b. In this simulation it can be seen that the electric field between the rearmost microchannel plate 3b and the second portion 12 of the collection anode 4 penetrates into the region between the rearmost microchannel plate 3b and first portion 10
30 of the collection anode 4. Accordingly, electrons released from the periphery of the rearmost microchannel plate 3b are accelerated back towards it and will not reach the collection anode 4. This can be seen from the

simulation to occur even though the first portion 10 of the collection anode 4 is maintained at a potential 58 kV higher than the rearmost microchannel plate 3b. Furthermore, the electric field penetration into the region between the rearmost microchannel plate 3b and first portion 10 of the collection anode 4 causes those electrons which are nonetheless transmitted to the collection anode 4 to be focussed onto a relatively small area of the first portion 10 of the collection anode 4. This may result in saturation of the detection system.

Fig. 7B shows a simulation of the electric potentials and electron trajectories 13 according to a preferred embodiment. The first portion 10 of the collection anode 4 is maintained at 17.75 kV and advantageously an additional lens system 8,9 is arranged between the microchannel plates 3a,3b and the collection anode 4. The lens system 8,9 preferably comprises three thin ring lens elements and a further annular ring lens element 9. The ring lens elements 8,9 are all preferably maintained at 17.75 kV. In this embodiment the presence of the lens system 8,9 substantially prevents the electric field between the rearmost microchannel plate 3b (which is maintained at 17 kV) and the second portion 12 of the collection anode 4 (which is maintained at 0 V) from penetrating into the region between the rearmost microchannel plate 3b and the first portion 10 of the collection anode 4. Therefore, the electrons released from the periphery of the rearmost microchannel 3b plate are not accelerated back onto it and so substantially all of the electrons emitted from the rearmost microchannel plate 3b are focussed onto the relatively small and distant collection anode 4.

Therefore, the potential difference between the rearmost microchannel plate 3b and first portion 10 of the collection anode 4 is significantly reduced whilst maintaining efficient electron transfer. In addition,
5 the lens system 8,9 prevents the electrons from being focussed onto a relatively small area of the first portion 10 of the collection anode 4 and so the electrons preferably do not cause saturation of the detection system.

10 The ion detector 1' according to the preferred embodiment comprises a collection anode 4 which is relatively small and distant from the microchannel plates 3a,3b. The collection anode 4 is decoupled from the recording device and the use of a lens system 8,9
15 enables the preferred ion detector 1' to function with lower electronic and ringing noise and with a higher bandwidth than a conventional ion detector 1. The ion detector 1' according to the preferred embodiment is also capable of detecting either positive or negative
20 ions in mass spectrometers having components upstream of the ion detector 1' which are maintained at various voltage configurations. Advantageously, the lens system 8,9 eliminates the need for an excessively high potential difference to be maintained between the
25 microchannel plates 3a,3b and the collection anode 4 in order to transport the electrons efficiently.

The reduction in capacitive coupling between the collection anode 4 and the microchannel plates 3a,3b results in a significant reduction in the level of
30 electronic noise pick-up and impedance mismatching between the collection anode 4 and the co-axial cable 6 leading to the Analogue to Digital Converter or the Time to Digital Converter.

Figs. 8A and 8B illustrate the mass spectra obtained for isotopes of a peptide having a molecular weight of 2564.2 measured using both a conventional ion detector 1 and an ion detector 1' according to the preferred embodiment. Fig. 8A shows the signal intensity as a function of mass to charge ratio for the analysis of positive ions of a peptide from the tryptic digest of alpha-casein in the molecular ion region. The data was acquired using a conventional Matrix Assisted Laser Desorption Ionisation axial Time of Flight mass spectrometer comprising a reflectron ("MALDI-R"). The mass spectrometer comprised a microchannel plate ion detector where the input surface of the collection anode 4 was arranged 14 mm behind the output surface of the microchannel plate. The resulting mass spectrum can be seen to show three distinct mass peaks with a relatively large amount of ringing noise also being observed. Fig. 8B shows a corresponding mass spectrum obtained using an ion detector 1' according to the preferred embodiment wherein the input surface of the collection anode 4 was arranged 32 mm behind the output surface of the rearmost microchannel plate 3b. In this embodiment the capacitive coupling between the collection anode 4 and the microchannel plate 3a,3b was significantly reduced. Correspondingly, the ringing noise after the detection of the first mass peak was significantly attenuated and as such a fourth distinct mass peak was observed above the noise which was substantially observed in the mass spectrum shown in Fig. 8A which was obtained using a conventional ion detector 1.

Fig. 9 shows the signal intensity as a function of mass to charge ratio for the analysis of negative ions of a peptide from the tryptic digest of alpha-casein

across the mass to charge ratio range of 1000-3500. The data was acquired using a Matrix Assisted Laser Desorption Ionisation Time of Flight mass spectrometer. The mass spectrometer comprised a preferred ion detector
5 1' similar to that illustrated in Fig. 7B.

Fig. 10 shows an embodiment comprising a dual microchannel plate assembly 3a,3b and a lens comprising an electro-magnet comprising a solenoid 14 wherein a portion of the anode 4 is placed within the solenoid 14.
10 When the solenoid 14 is energised a magnetic field is generated as indicated by the dashed lines. The dashed lines indicate the magnetic field lines, and the magnetic field may be in either direction. Electrons released from the output face of the rearmost
15 microchannel plate 3b may be arranged to have relatively low energies, typically up to about 100 eV. Low energy electrons released from the output face of the microchannel plate 3b will spiral about the lines of magnetic field. It can be seen from the figure that the
20 lines of magnetic field become more concentrated in the centre of the solenoid 14, and so electrons from a broad area outside the solenoid 14 may be brought to a smaller area within the solenoid 14. A relatively small anode 4 may be placed within the solenoid 14 to collect the
25 electrons. The anode 4 may be made of a non-magnetic conducting material. Alternatively, the anode 4 may be made of a soft magnetic material such as iron, mild steel, or various silicon-iron, nickel-iron or cobalt-iron alloys preferably having a relatively low
30 coercivity less than 1000 Amp/meter. The soft magnetic material will further concentrate the magnetic field in the region of the anode 4.

Fig. 11 shows another embodiment comprising a dual microchannel plate assembly 3a,3b and an anode 4 made from a permanent magnet which preferably has a relatively high coercivity of at least 3000, 3500 or 4000 Amp/meter. The figure shows the north pole of the magnetised anode 4 facing the microchannel plate assembly 3a,3b. Alternatively, the detector 1' may be arranged so as to have the south pole of the magnet facing the microchannel plate assembly 3a,3b. The dashed lines indicate the direction of the lines of the magnetic field. Electrons released from the output face of the rearmost microchannel plate 3b are preferably arranged to have relatively low energies, typically up to about 100 eV. Low energy electrons released from the output face of the microchannel plate 3b will preferably spiral about the lines of magnetic field. Since all the magnetic field lines pass through the permanently magnetised anode 4 then all the low energy electrons will be directed towards the magnetised anode 4. The anode 4 is preferably made of a hard or permanent (high coercivity) magnetic material such as carbon steel, cobalt steel, chrome steel and tungsten steel. Alternatively, the anode 4 may be made from various alloys, such as alloys of iron with aluminium, nickel and cobalt, or with aluminium, nickel, cobalt and copper. Alternatively, the anode 4 may be made from various rare earth element alloys, including rare earth element alloys with cobalt. For example, the anode 4 may be made of an alloy of cobalt and praseodymium, or an alloy of cobalt, cerium, copper and iron.

Further embodiments are contemplated wherein the anode 4 in the embodiment shown in Fig. 10 may also be permanently magnetised and one or more electrodes and/or

further magnetic lenses may be provided to direct electrons on to the anode 4. Similarly, one or more electrodes and/or magnetic lenses may be provided to help direct electrons on to the permanently magnetised anode 4 in the embodiment shown in Fig. 11.

Whilst the various embodiments have been described in relation to using two microchannel plates 3a,3b it is also contemplated that either a single or alternatively more than two microchannel plates may be provided. Similarly, it is also contemplated that the ion detector 1' may be incorporated in mass spectrometers other than Time of Flight mass spectrometers.

Although the present invention has been described with reference to preferred embodiments, it will be understood by those skilled in the art that various changes in form and detail may be made without departing from the scope of the invention as set forth in the accompanying claims.